# Enhancement The Dynamic Stability of The Iraq's Power Station Using PID Controller Optimized by FA and PSO Based on Different Objective Functions

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**Abstract**. The paper demonstrates how to improve the dynamic stability of a synchronous generator in combination with on excitation system by utilizing a Proportional Integral Derivate (PID) controller. It presents two methods of determining optimal the PID parameters to improve the power angle and terminal voltage of a synchronous generator: i.e. the Firefly Algorithm (FA) and Particle Swarm Optimization (PSO). These methods are used to determine the optimal PID controller parameters required to minimize various performance indices as objective functions. Two objective functions are considered for optimization: the Integral Absolute Error (IAE) and the Integral Error (ISE). The results obtained from conventional PID, FA-PID and PSO-PID, it shows that the FA-PID performed better than the conventional PID and PSO-PID. The result analysis demonstrates that FA-IAE better and more efficient by tune the PID parameters than FA-ISE, PSO-IAE and PSO-ISE.

**Keywords**: dynamic stability; excitation system; Firefly Algorithm (FA); PID controller; Particle Swarm Optimization (PSO); objective functions

#### Izboljšava dinamične stabilnosti sinhronskega generatorja z uporabo krmilnika PID in optimizacijskih metod FA in PSO

V prispevku smo predstavili izboljšanje dinamične stabilnosti sinhronskega generatorja v kombinaciji z vzbujevalnim sistemom z uporabo krmilnika PID. Uporabili smo algoritem obnašanja kresnic (FA) in optimizacije rojev delcev (PSO) pri določitvi optimalnih parametrov krmilnika PID za izboljšanje kota moči in priključne napetosti sinhronskega generatorja. Z obema algoritmoma smo določili optimalne parametre PID za minimizacijo različnih indeksov zmogljivosti. Za optimizacijo smo uporabili dve kriterijski funkciji. Eksperimentalno smo potrdili, da z algoritmom FA-PID dobimo boljše rezultate kot z algoritmom FA-PSO in konvencionalnim krmilnikom PID.

## **1 INTRODUCTION**

The study of the dynamic stability of modern power systems is one of the most important challenges. The power system control is to maintain a reliable and quality supply power. The power system is stable when there is a balance between the power demand and the power generated [1, 2]. The constants needed to coordinate the operation between of synchronous generator connected to infinite bus bar and on excitation system were developed by [3] and then by [4].

Power system problems are still solved by utilizing the PID type controller. In optimal PID tuning gains is required, under different operating states, to get the In the paper we present results of our study of the dynamic stability of a synchronous generator combined with an excitation system and utilization of FA and PSO for tuning the PID parameters to minimize two different objective functions, i.e. the Integral Absolute Error (IAE) and the Integral Square Error (ISE).

# 2 MODELING OF A SYNCHRONOUS GENERATOR COMBINED WITH ON EXCITATION SYSTEM

In [3] and [4], the coupling effects of the synchronous generator and the excitation system are described. The dynamic stability of the Iraqi Derbindikhan power plant combined with an AVR system is studied. Figure 1 shows the transfer function model of a synchronous generator coupled with an AVR system. The relevant parameters are presented in Table 1. According to [9, 10], the following equations are used for coupling:

$$\Delta T_{\rm e} = K_1 \Delta \delta + K_2 \Delta E_{\rm q}^{\prime} \tag{1}$$

$$\Delta E'_{q} = \frac{K_{3}}{1 + K_{3} T'_{d0} s} \Delta E_{FD} - \frac{K_{3} K_{4}}{1 + K_{3} T'_{d0} s} \Delta \delta$$
(2)

$$\Delta V_{t} = K_{5} \Delta \delta + K_{6} \Delta E_{q}^{'} \tag{3}$$

desired level of robust performance. For on optimal PID tuning, a Particle Swarm Optimizer (PSO) is used in [5, 6]. In [7, 8] using the Firefly Algorithm (FA), the optimal PID tuning is implemented.

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Figure 1. MATLAB/Simulink model of the Generator and AVR system.

Table 1.	Parameters	of	the	synchronous	generator	and	AVR
system.							

Parameters of the	Parameters of the AVR
synchronous generator	system
$R_{e} = 0.00407$	$K_{A} = 50$
$X_{e} = 0.2037$	$T_{A} = 0.06$
$X_{d} = 1.2$	$K_E = 1$
$X_{q} = 0.69$	$T_{E} = 0.46$
$X'_{d} = 0.38$	$K_{\rm F} = 0.1$
$T_{do}^{''} = 5.14$	$T_F = 1$
$T_{m} = 1.059$	$S_{E1} = 0.0039$
M = 9.4	$S_{E2} = 1.555$
D = 1	$V_{ref} = 1.0282$

Constants  $K_1 - K_6$  are calculated using the following equations:

$$\begin{split} & K_{1} = \frac{V_{\infty}I_{q}(X_{q} - X'_{d})}{R_{e}^{2} + (X_{e} + X_{q})(X_{e} + X'_{d})} \Big[ (X_{e} + X_{q}) \sin \delta - R_{e} \cos \delta \Big] + \\ & \frac{V_{\infty}I_{d}(X_{q} - X'_{d})}{R_{e}^{2} + (X_{e} + X_{q})(X_{e} + X'_{d})} \Big[ (X_{e} + X'_{d}) \cos \delta + R_{e} \sin \delta \Big] + \\ & \frac{V_{\infty}E'_{q}}{R_{e}^{2} + (X_{e} + X_{q})(X_{e} + X'_{d})} \Big[ (X_{e} + X'_{d}) \cos \delta + R_{e} \sin \delta \Big] \\ & (4) \\ & K_{2} = \frac{1}{R_{e}^{2} + (X_{e} + X_{q})(X_{e} + X'_{d})} \Big[ I_{q} \left( R_{e}^{2} + \left( X_{e} + X_{q} \right)^{2} \right) + \\ & I_{d}R_{e} (X_{q} - X'_{d}) + E'_{q}R_{e} \Big] \end{aligned}$$
(5)

$$K_{3} = \frac{R_{e}^{+}(X_{e} + X_{q})(X_{e} + X_{d})}{R_{e}^{2} + (X_{e} + X_{q})(X_{e} + X_{d})}$$
(6)

$$K_4 = \frac{v_{\infty}(X_d - X_d)}{R_e^2 + (X_e + X_q)(X_e + X_d)} \left[ \left( X_e + X_q \right) \sin \delta - R_e \cos \delta \right]$$
(7)

$$\begin{split} K_{5} &= \frac{V_{\infty}V_{d}X_{q}}{V_{t}[R_{e}^{2}+(X_{e}+X_{q})(X_{e}+X_{d}^{'})]} \Big[ \left(X_{e}+X_{d}^{'}\right)\cos\delta + \\ R_{e}\sin\delta \Big] - \frac{V_{\infty}V_{q}\dot{X_{d}}}{V_{t}[R_{e}^{2}+(X_{e}+X_{q})(X_{e}+X_{d}^{'})]} \Big[ \left(X_{e}+X_{q}\right)\sin\delta - \\ R_{e}\cos\delta \Big] \end{split}$$
(8)

$$K_{6} = \frac{1}{V_{t}[R_{e}^{2} + (X_{e} + X_{q})(X_{e} + X_{d}^{'})]} \left[ V_{d}X_{q}R_{e} + V_{q} \left( R_{e}^{2} + X_{e} \left( X_{e} + X_{q} \right) \right) \right]$$
(9)

## 3 MODELING OF THE PID CONTROLLER

Due to its uncomplicated and simple implementation, the PID controller is one of the most successful efficient and widely used control instrument in the industry. Based on [8, 11], Figure 2 shows a typical structure of the conventional PID controller.



Figure 2. Block diagram of the PID controller.

The transfer function of the PID controller described with regard to the Laplace domain is:

$$G_{PID}(s) = \frac{U(s)}{E(s)} = k_p + \frac{k_i}{s} + k_d s$$
 (10)

where U(s) is the control signal and E(s) is the error signal. These are the difference between the input and feedback.  $k_p$  is the proportional gain,  $k_i$  is the integration gain and  $k_d$  is the derivative gain.

The output of the PID controller in terms of the time domain is:

$$u(t) = k_p e(t) + k_i \int_0^t e(t) dt + k_d \frac{de(t)}{dt}$$
(11)

where u(t) is the control error signal and e(t) is the tracking error signal; both are in the form of the time domain.

The effect of the IAE and ISE objective functions on optimization parameter is studied. The IAE and ISE functions are defined as:

IAE = 
$$\int_{0}^{1} [|e_1(t)| + |e_2(t)|] dt$$
 (12)

ISE = 
$$\int_0^t [(e_1)^2(t) + (e_2)^2(t)] dt$$
 (13)

The optimization functions IAE and ISE are minimized and subjected to:

$$\begin{aligned} k_p^{\min} &\leq k_p \leq k_p^{\max} , \ k_i^{\min} \leq k_i \leq k_i^{\max} \text{ and } \\ k_d^{\min} &\leq k_d \leq k_d^{\max} \end{aligned} \tag{14}$$

### **4 OPTIMIZATION TECHNIQUES**

Our main objective is to control the power angle and terminal voltage of the Derbindikhan power plant by using modern heuristic techniques which play an important role in controlling the power system performance. Conventional by the first step is to tune the controller parameters which is, unfortunately, not applicable in practical systems. As a result, powerful mathematical optimization methods are used for PID parameters tuning. The most reliable ones, i.e. PSO and FA, are population-based optimization techniques.

#### 4.1. Firefly Algorithm (FA)

Developed by Xin She Yang in 2007, FA is based on the natural swarming behavior of animals such as schools of fish, swarms of insects and birds. Regarding the social light-flashing ability of fireflies (or lighting bugs) in the skies of tropical regions, FA is a metaheuristic optimization algorithm inspired by nature [12, 13]. FA has three idealized rules based on some of the main flashing abilities of fireflies. They are:

- a. Being unisex, fireflies are drawn to more attractive, brighter, individuals regardless of their sex.
- b. The firefly's brightness is directly related to the degree of its attractiveness. The brighter it is the more attractive it is to other fireflies. As its distance from the fireflies increases, its brightness diminishes. This is because the air absorbs its light. If no firefly shines brighter than an individual firefly in the vicinity, it will move about at random.
- c. The value of the objective function of a given problem determines the brightness or the intensity of the light a firefly emits. For optimization problems, the value of the objective function is proportional to the

intensity of light. The following equations describe implementation of FA:

$$X_{i}^{\text{new}} = X_{i}^{\text{old}} + \beta \left( X_{j} - X_{i} \right) + \alpha \left( \text{rand} - \frac{1}{2} \right)$$
(15)

The firefly movement is represented by equation (15). The first term is the firefly's current position. The second term represents the firefly's attraction to the light intensity. The third term describes the firefly's motion when there are no brighter fireflies. Coefficient  $\alpha$  is a randomization parameter determined by the problem of interest while rand is a random number generator uniformly distributed in space [0, 1].

$$\beta = \beta_0 e^{-\gamma r_{ij}^m} \qquad (m \ge 1) \tag{16}$$

where *r* is the distance between any two fireflies,  $\gamma$  is an absorption coefficient that regulates the decrease of the light intensity  $\beta_0$  is the initial attractiveness at r = 0.

$$r_{ij} = \|X_i - X_j\| = \sqrt{\sum_{k=1}^{d} (X_{i,k} - X_{j,k})^2}$$
(17)

Term  $X_{i,k}$  is the kth component of spatial coordinate  $X_i$  of the ith firefly; d is the number of dimensions. Figure 3 shows a flowchart of the FA-PID based on the IAE or ISE objective.

#### 4.2. Particle Swarm Optimization (PSO)

Kennedy and Eberhart developed PSO, a modern heuristic algorithm in 1995 [14]. It effectively solves in the PSO method, continuous and nonlinear optimization problems. A swarm made up of individuals called particles is defined by its velocity and position [5, 15].

Every particle in the swarm knows the global best  $(g_{best})$ , i.e. the location with the best objective value in the swarm. Each particle at each point along its path, compares the objective value of its personal best  $(p_{best})$  to that of  $(g_{best})$ . If a particle has a  $(p_{best})$  that has a superior objective value than the current $(g_{best})$ , the current  $(g_{best})$  is replaced with that particle's  $(p_{best})$ . Its movement is halted when all particles approach a position in the swarm with the best objective function. By updating the positions and velocities of particles, the algorithm can search for an optimum solution in a specified search space. The following equation is what each particle utilizes to initialize its positions and velocities:

$$X_{i}^{k+1} = X_{i}^{k} + V_{i}^{k+1}$$
(18)

$$V_{i}^{k+1} = wV_{i}^{k} + c_{1}r_{1}(p_{\text{best }i}^{k} - X_{i}^{k}) + c_{2}r_{2}(g_{\text{best }i}^{k} - X_{i}^{k})$$
(19)

$$w = \frac{\text{maxiter-iter}}{\text{maxiter}}$$
(20)

Where  $X_i^k$  is the position of a particle at a k iteration,  $X_i^{k+1}$  is the position of a particle at a k+1 iteration,  $V_i^k$  is the velocity of a particle at a k iteration,  $V_i^{k+1}$  is the velocity of a particle at a k+1 iteration, w is the inertia weight parameter, ,  $r_1$  and  $r_2$  are a random number in the interval;  $c_1$  and  $c_2$  are the learning factors [0, 1]. Figure 3 shows a flowchart of PSO-PID based on AIE or ISE objective function.



Figure 3. Flowchart of FA or PSO for the PID controller.

#### **5 RESULTS AND DISCUSSION**

Figure 4 shows a synchronous generator model connected to an AVR system and implemented with a PID controller in a MATLAB/Simulink. Figure 5 shows the results of a power angle simulation first carried out with and with no PID controller. Figure 6 shows the terminal voltage with and with no PID controller. The values of the PID controller obtained with the conventional method are shown in Table 2. The graphs are shown only for the first 50 seconds for the power angle and for 10 seconds for the terminal voltage though the simulation took 60 seconds. Table 3 shows the maximum peak, setting time, minimum peak and

final value for the power angle. Table 4 shows the maximum deviation, peak time, settling time and steady state error for the terminal voltage.



Figure 4. MATLAB/Simulink model of the Generator and AVR system with a PID controller.



Figure 5. Power angle with and with no PID controller.



Figure 6. Terminal voltage with and with no PID controller.

PID Parameters	<b>Conventional method</b>
K <sub>p1</sub>	1.9943
K <sub>i1</sub>	0.0022
K <sub>d1</sub>	1.3216
K <sub>p2</sub>	2.3850
Kiz	0.0098

Table 2. Values of the PID controller with conventional method.

Table 3.	Power	angle	characteristics	with	and	with	no	PID
controller	•							

K 4

0.5511

	With no PID	Conventional PID
Max. peak (Deg.)	18.51	14.85
Min. peak (Deg.)	-21.12	-14.76
Settling time (sec.)		31.9
Final value (Deg.)	-8.256	-5.877

Table 4. Terminal voltage characteristics with and with no PID controller.

	With no PID	Conventional PID
Max. deviation (p.u)	1.16	1.117
Peak time (sec.)	3.161	3.135
Settling time (sec.)	4.041	3.934
Steady state error (p.u)	-0.0118	-0.0068

Different algorithms have been implemented for turning the k<sub>p</sub>, k<sub>i</sub> and k<sub>d</sub> gains of the PID controller to improve the performance of the synchronized generator coupled with on AVR system. Three is the upper and zero is the lower limit value of the PID controller. First, the optimal value of the PID controller as an objective function is determined by using the IAE performance index value, i.e. the sum of absolute cumulative errors shown in Figure 7. Second, the ISE performance index, i.e. the sum of the square of cumulative errors, is used to determine optimal values of the PID controller as an objective function shown in Figure 8. To minimize IAE and ISE, FA-IAE, FA-ISE, PSO-IAE and PSO-ISE, i.e. optimized combinations, are used. The optimal PID controller tuning gains for the combinations sets are shown in Table 5.



Figure 7. MATLAB/Simulink model of the Generator and AVR system based on IAE.



Figure 8. MATLAB/Simulink model of the Generator and AVR system based on ISE.

Table 5. Optimal PID controller gains.

PID Parameter	PSO-IAE	PSO-ISE	FA-IAE	FA-ISE
S				
K <sub>p1</sub>	2.2894	2.9838	1.8856	2.5527
K <sub>i1</sub>	0.0751	0.0990	0.0521	0.0661
K <sub>d1</sub>	2.7298	2.9738	2.4600	2.6150
K <sub>p2</sub>	2.8285	1.9284	2.6322	1.5893
K <sub>i2</sub>	0.0118	0.0121	0.0102	0.0086
K <sub>d2</sub>	0.9310	0.4696	0.9156	0.3834

Figure 9 shows the response of the power angle obtained by using FA and PSO. Figure 10 shows The response of terminal voltage obtained by using FA and PSO. The graphs for the power angle are displayed for the first 50 seconds and 10 seconds for the terminal voltage though the simulation took 60 seconds. The maximum peak, minimum peak, settling time and final value of the power angle are shown in Table 6. The maximum deviation, peak time, settling time and steady state error for the terminal voltage are presented in Table 7.



Figure 9. Power angle with PID tuning by FA and PSO.



Figure 10. Terminal voltage with PID tuning by FA and PSO.

	FA- IAE	FA-ISE	PSO- IAE	PSO-ISE
Max. peak (Deg.)	7.796	12.28	9.884	13.95
Min. peak (Deg.)	-9.062	-11.25	-9.396	-11.54
Settling time (sec.)	28.07	28.17	28.11	28.25
Final value (Deg.)	-5.357	-5.517	-5.454	-5.624

Table 6. Power angle characteristics with PID tuning by using FA and PSO.

Table 7. Terminal voltage characteristics with PID tuning by using FA and PSO.

	FA-IAE	FA-ISE	PSO- IAE	PSO- ISE
Max. deviation (p.u)	1.06	1.08	1.075	1.099
Peak time (sec.)	3.025	3.064	3.068	3.071
Settling time (sec.)	3.642	3.853	3.767	3.895
Steady state error (p.u)	-0.0049	-0.0056	-0.0051	-0.0064

Figure 11 shows the minimization convergence of the IAE index by using FA and PSO to determine the optimal values of the PID controller. Figure 12 presents the minimization convergence of the ISE index by using FA and PSO to determine the optimal the PID controllers values. The FA-FID controller performed better than the PSO-PID controller as shown by the convergence curves.

The overall characteristics of the power angle and terminal voltage in the above results are reduced by FA and PSO for PID controller tuning. The power system damping characteristics compared to conventional PID controller, are more effectively improved by using FA and PSO for PID controller tuning. The power system oscillations are reduced, and its stability is preserved.



Figure 11. Convergence curve of FA and PSO based on IAE to obtain the PID parameters.



Figure 12. Convergence curve of FA and PSO based on ISE to obtain the PID parameters.

#### **6 CONCLUSIONS**

In the paper we study the dynamic stability of a synchronous generator with an excitement system whose performance is enhanced by using a PID controller. To tune the optimal values of the PID controller, the FA and PSO algorithms are used indicating effectiveness and robustness of the proposed approach for the IAE and ISE objective functions. The results are compared with FA-PID and conventional PID, PSO-PID. To determine the PID controller gains with respect to the overall performance characteristics of the power angles and terminal voltage of the Derbindikhan power plant, our comparison shows that FA is more efficient and promising for determination the PID controller gains. As to objective functions our results show that the response performance of the IAE criterion is more promising than ISE criterion.

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